

### Location Restrictions Demonstrations

DTE Electric Company Monroe Power Plant Fly Ash Basin Coal Combustion Residual Unit

> 7955 East Dunbar Road Monroe, Michigan

September 2018



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Prepared For DTE Electric Company

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TRC | DTE Electric Company
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## Certification

I, the undersigned Michigan Professional Engineer, hereby certify that I am familiar with the technical requirements of Title 40 Code of Federal Regulations Part 257 Subpart D (§257). I also certify that it is my professional opinion that, to the best of my knowledge, information, and belief, that the information in this demonstration is in accordance with current good and accepted engineering practice(s) and standard(s) and meets the requirements of §257.60 through §257.64.

For the purpose of this document, "certify" and "certification" shall be interpreted and construed to be a "statement of professional opinion." The certification is understood and intended to be an expression of my professional opinion as a Michigan Licensed Professional Engineer, based upon knowledge, information, and belief. The statement(s) of professional opinion are not and shall not be interpreted or construed to be a guarantee or a warranty of the analysis herein.

David B. McKenzie, P.E.	
License No: 6201042332	
	Seal/Date

## Section 1 Background

The purpose of this document is to demonstrate that the Coal Combustion Residual (CCR) Fly Ash Basin (FAB) at the Monroe Power Plant (MONPP) is in compliance with the location restrictions outlined in the Environmental Protection Agency's (EPA) final CCR rule [Title 40 Code of Federal Regulations Parts 257 and 261] Subpart D – "Standards for the Disposal of Coal Combustion Residuals in Landfills and Surface Impoundments" (§257.60 through §257.64, federal rule). The FAB is considered a CCR impoundment and landfill.

This document includes information from a desktop study and well installation activities and also engineering calculations to demonstrate that the FAB is in compliance with placement above the uppermost aquifer criteria (§257.60), and location criteria with respect to wetlands (§257.61), fault areas (§257.62), seismic impact zones (§257.63), and unstable areas (§257.64).

Supporting documents are provided as appendices to this demonstration.

#### 1.1 Facility and CCR Unit Information

The MONPP is located in Section 16, Township 7 South, Range 9 East, at 7955 East Dunbar Road, Monroe in Monroe County, Michigan. The MONPP FAB is located about one mile southwest of the MONPP at latitude 41° 53' 03" North and longitude 83° 22' 31" West. The MONPP FAB is bounded by Dunbar Road and Plum Creek to the north and northeast, Interstate 75 to the northwest, a 200-acre peninsula into Lake Erie to the east and southeast, Lake Erie to the south and a large open field to the southwest.

The property has been used continuously for the operation of the MONPP FAB since approximately 1975 and is constructed over a natural clay-rich soil base. The MONPP FAB and landfill is a Type III solid waste disposal facility owned by DTE Electric Company (DTE Electric), which currently accepts coal ash from DTE Electric's MONPP. The MONPP FAB is operated in accordance with Michigan Part 115 of the Natural Resources and Environmental Protection Act (NREPA), PA 451 of 1994, as amended, and the current operating license number is 9393.

The FAB base is keyed into the existing natural clay-rich soil ground surface at an elevation of 563.4 feet. This natural low permeability clay-rich soil base serves as an underlying hydraulic barrier, forming a natural liner of at least 23 feet of natural clay-rich soil below the base of the FAB. The constructed berm that follows the perimeter of the FAB reaches an elevation of 614 ft., approximately 5 ft above the operational water level of the FAB.

### 1.2 Site Setting

The MONPP FAB CCR unit is located approximately 200 feet southwest of Plum Creek and immediately north of Lake Erie. The uppermost aquifer at the MONPP FAB CCR consists of saturated limestone present beneath at least 37 feet and up to 53.5 feet of thick contiguous silty clay-rich soil that serves as a natural confining hydraulic barrier that isolates the underlying uppermost aquifer. The limestone bedrock aquifer is artesian in every location except MW-16-01, where the static water level was approximately 1 to 2 feet below ground surface (ft bgs).

A groundwater monitoring system has been established for the MONPP FAB CCR unit as detailed in the *Groundwater Monitoring System Summary Report – Monroe Power Plant Coal Combustion Residual Fly Ash Basin* (GWMS Report) (TRC, October 2017). The detection monitoring well network for the MONPP FAB CCR unit currently consists of seven monitoring wells that are screened in the uppermost aquifer. The monitoring well boring logs are included in Appendix A.

A mean hydraulic conductivity of approximately 4.3 feet/day was measured from one of the CCR monitoring wells using single well hydraulic conductivity tests (e.g., slug tests) performed in 2016. This result is consistent with other sources (5 feet/day) for the hydraulic conductivity of the Bass Island Group.

Potentiometric groundwater elevation data collected in 2016 and 2017 suggest that there is horizontal groundwater flow potential within the upper aquifer unit generally to the northeast towards Plum Creek. The average hydraulic gradient to the northeast is on the order of 0.002 foot/foot along the eastern part of the MONPP FAB to 0.004 to 0.005 foot/foot in the center and northwestern part of the FAB, with an overall mean gradient of 0.004 foot/foot.

The surface water elevation within the FAB raised surface impoundment is at least 5 to more than 30 feet above the potentiometric surface elevations in the uppermost aquifer limestone, and more than 60 feet above the base of the underlying clay-rich confining unit that isolates groundwater within the limestone aquifer. Therefore, flow potential from the CCR unit to the surrounding area would be radially outward from the FAB. However, there is no hydraulic communication between the uppermost aquifer and the FAB due to the continuous silty clay-rich confining unit beneath the MONPP FAB. Based on the artesian conditions, the low permeability of the underlying natural soils, and the calculated time of travel for groundwater to flow vertically from the FAB to the uppermost aquifer, it is not possible for the uppermost aquifer to have been affected by CCR from FAB operations that began in 1975.

## Section 2 Location Restrictions

The location restrictions designated in the federal CCR rule are presented below with a corresponding demonstration to show compliance with each restriction. The location restrictions include placement above the uppermost aquifer, within wetlands, near fault areas, within seismic impact zones, and unstable areas based on available geologic and geomorphological information. Supporting information for the demonstrations is included in the appendices to this report.

### 2.1 §257.60 – Placement Above the Uppermost Aquifer

The federal CCR rule requires that CCR units such as the MONPP FAB must be constructed with a base that is located no less than 1.52 meters (five feet) above the upper limit of the uppermost aquifer, or must demonstrate that there will not be an intermittent, recurring, or sustained hydraulic connection between any portion of the base of the CCR unit and the uppermost aquifer due to normal fluctuations in the groundwater elevations (including the seasonal high water table). As discussed in Section 1.1 (above), the FAB is keyed into the natural clay-rich soil ground surface at an elevation of 563.4 feet. THE FAB is underlain by at least 23 feet of the natural low permeability clay-rich soil. The uppermost aquifer, based on saturated soil observations during soil borings is located at the silty clay-weathered limestone interface, at an approximate elevation of 527 to 540 ft MSL. Cross-sections showing the installation top and bottom elevation of the approximate basin bottom and depth to the uppermost aquifer are included in Appendix B.

Based on this demonstration, the base of the MONPP FAB is located greater than 5 feet above the upper limit of the uppermost aquifer and there is not a hydraulic connection between the FAB and the underlying groundwater caused by normal fluctuations in groundwater level. Therefore, the FAB is in compliance with the requirements of §257.60.

#### 2.2 §257.61 – Wetlands

The CCR location standards restrict existing and new CCR surface impoundments from being located in wetlands, as defined at 40 CFR 232.2 (40 CFR 257.61(a)). Wetlands are defined in 40 CFR 232.2 *Waters of the United States* (3)(iv) as, "...those areas that are inundated or saturated by surface or groundwater at a frequency and duration sufficient to support, and that under normal circumstances do support, a prevalence of vegetation typically adapted for life in saturated soil conditions. Wetlands generally include swamps, marshes, bogs, and similar areas." TRC reviewed National Wetland Inventory (NWI) maps and Michigan Resource Information

System (MIRIS) Land Cover Maps archived and available through Michigan Department of Natural Resources (MDNR), Michigan Resource Inventory Program (MRIP) to ascertain whether or not the MONPP FAB located in wetlands.

As shown on the map in Appendix C, soils at and in the vicinity of the site are designated as wetland soils, most likely due to the proximity of the site to Plum Creek and Lake Erie. NWI (2005) recognizes areas to the southeast and northeast of the FAB as wetlands, and an area identified as wetlands on NWI and MIRIS maps that has wetland soils is located within the site. However, wetland delineations performed at the MONPP FAB by DTE Electric showed that all wetlands were located outside of the FAB berms (outside the CCR unit) in perimeter drainage channels.

Based on TRC's review of wetland inventory resources and current site conditions, TRC is of the opinion that the MONPP FAB is not located in an area exhibiting wetland characteristics, and that continued operations at the FAB will have no potential to impact any wetlands near the CCR unit. TRC also concludes that due to its use as an NPDES treatment unit, this basin is not wetlands as defined in 40 CFR 232.2.

#### 2.3 §257.62 – Fault areas

The federal CCR rule requires that CCR units not be located within 60 meters (200 feet) of the outermost damage zone of a fault that has had displacement in Holocene time (within the most recent 11,700 years) unless the owner or operator demonstrates that an alternative setback distance of less than 60 meters (200 feet) will not cause damage to the structural integrity of the CCR unit. USGS-recognized Quaternary faults in the U.S. are shown on the map in Appendix D.

The lower peninsula of Michigan is covered by a mantle of glacial deposits obscuring any surficial evidence of faulting (Bricker, 1977). In these areas of glacial deposition, fault zones are considered to be stable, and any recent recorded earth movement in Michigan has been noted to originate from source depths of 95 to 110 kilometers into the subsurface (Brinker, 1977). Historical records indicate that nearly all seismic events that have occurred in Michigan have been relatively minor in intensity (I to VI on the Modified Mercalli Intensity Scale).

Evidence of active faulting during the Holocene in the MONPP FAB area is not supported by this determination; therefore, the FAB is in compliance with the requirements of §257.62.

### 2.4 §257.63 – Seismic Impact Zones

The federal CCR rule requires that CCR units not be located in seismic impact zones unless the owner or operator demonstrates that all structural components including liners, leachate collection and removal systems, and surface water control systems, are designed to resist the

maximum horizontal acceleration in lithified earth material for the site. The federal CCR rule defines a seismic impact zone as "an area having a 2% or greater probability that the maximum expected horizontal acceleration, expressed as a percentage of the earth's gravitation pull (g), will exceed 0.10 g in 50 years."

To determine whether the MONPP FAB is located in a seismic impact zone, the USGS Earthquake Hazards Program was consulted to determine the earthquake hazard for the FAB. The Earthquake Hazards Program uses the 2015 NEHRP Provisions as a reference document; the following factors were used to calculate the peak ground acceleration:

- The site class is Class C: firm to very stiff surficial clay soils underlain by very stiff to hard clay beginning at approximately 20 ft bgs. The clay is underlain by weathered and competent limestone bedrock beginning approximately 30 to 50 ft bgs. This determination was made based on the first 100 ft of soil and rock encountered. The first 50 feet are comprised of very stiff to hard clay, and the remainder is limestone bedrock.
- The site falls under the Risk Category III, due to its primary function as a power-generating station.

The 2015 National Earthquake Hazards Reduction Program U.S. seismic design maps website (USGS 2015; Appendix E) indicates a mapped peak ground acceleration of 0.063 g for the FAB area. Using the Class C site determination results in a design peak ground acceleration of 0.082 g. This calculated design peak ground acceleration value is less than 0.10 g in 50 years.

Evidence of a seismic impact zone is not supported by this determination; therefore, TRC concludes that the MONPP FAB is not located in a seismic impact zone. The FAB is in compliance with the requirements of §257.63.

#### 2.5 §257.64 – Unstable Areas

The federal CCR rule requires that CCR units not be located in an unstable area unless the owner or operator demonstrates that recognized and generally accepted good engineering practices have been incorporated into the design of the CCR unit to ensure that the integrity of the structural components of the CCR unit will not be disrupted. Factors associated with soil conditions resulting in significant differential settlement, geologic or geomorphologic features, and human-made features or events must be evaluated to determine compliance.

This demonstration was performed by evaluating the results of geotechnical explorations at the MONPP (Geosyntec Consultants, 2010), the Round 7 Dam Assessment-Final Report (GZA GeoEnvironmental, Inc., 2011), reviewing local geology and topography, and evaluating human-made features or events at the MONPP area.

The geotechnical exploration performed at the MONPP identified silty clay, with traces of sand and gravel. The clay exhibits a very stiff to hard consistency and high shear strengths, with harder and stronger soils noted with depth. The unconsolidated soils occur above weathered and competent limestone bedrock. Based on these geotechnical records, there is no evidence of unstable soil or underlying bedrock conditions proximal to the FAB.

Based on information maintained by the Michigan Natural Features Inventory and Michigan State University Extension, Monroe County topography, due to the presence of underlying limestone bedrock, is subject to the potential but infrequent occurrence of sinkholes and caves. However, no evidence of sinkholes or caves have been discovered or noted at the MONPP property and therefore are not expected to contribute to the development of unstable site soil conditions.

Based on DTE Electric records, the perimeter berm for the FAB was constructed in the 1970s. In 2016, Geosystec Consultants performed a slope stability safety factor assessment for the FAB berms (Geosyntec, 2016). The assessment concluded that the Ash Basin meets the safety factor requirements with the maximum water level maintained at 609 ft MSL or less.

Evidence of unstable areas due to soil conditions resulting in significant differential settling, geologic or geomorphologic features, or human-made features or events is not supported by this determination; therefore, it is TRC's opinion that MONPP FAB is not located in an unstable geological area and that the FAB berm meets safety factor requirements at current FAB operating conditions and berm structural conditions. The FAB, therefore, is in compliance with the requirements of §257.64.

## Section 3 Conclusions

Based on the evaluation provided in this demonstration, the MONPP FAB is in compliance with the location restrictions provided in §257.60 through §257.64 of the CCR rule. No additional action, justification, or demonstration is required to document compliance with the location restrictions provided in the CCR rule after this demonstration has been placed into the operating record, posted to the publicly-accessible website, and government notifications provided.



## Section 4 References

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# Appendix A Monitoring Well Boring Logs



Facili	ty/Projec	ct Name			50.777.7	S.W		Date Drilling Starte	d:	Date		Complete	ed:	Projec	1 of 1 ot Number:
				DTE EC:	Monroe F			2/17/16	11-2-2			7/16		10000	828.0001.000
Drillin	g Firm:				Drilling Me			Surface Elev. (ft)		Elevation		Total D		it bgs)	Borehole Dia. (in
Rorin			Drillin	g ash basin.		Sonic	3	578.91 Personnel		581.7	4	Drilling	60.0	ment.	6
SOLILI	g Locali	on. Sv	v or ny	asn basin.				Logged By - Jenn	ifer Ree	d		Dilling			4.7
				4675.84		Lacro		Driller - Austin Go						Terra	Sonic
	Fown/Ci			County:		State:		Water Level Obser While Drilling:		e/Time				Dept	th (ft bgs)
	Monro	e, M		N	lonroe	N	lichigan	After Drilling:	Dat	e/Time	3/17/	16 08:45	_ 1	Depl	th (ft bgs) 2.00
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И			-	Chan	Change to madium placticity, dark gray (10VP 4/1) mattled with										
2 CS	95		-	yellow	Change to medium plasticity, dark gray (10YR 4/1) mottled with yellowish brown (10YR 5/6), at 12.5 feet.										
CS	00		Ť												
			1	Chan	ge to dark	gray (10Y	R 4/1), very s	stiff at 17.5 feet.							
3			20 -								111				
3 ST	60														
											-				
4	100										CL-				
CS	100														
			30 -									W			
5 CS	100			Chan 7/1), s	ge to weat slight odor	hered lime , stiff at 32	stone appea .5 feet.	rance, light gray	(10YF	2					
			40 -												
6 CS	95			Chan		silt, few co	arse sand at	43.5 feet. d at 45.0 feet.							
					es to wet fr ge to bedr			ered, wet at 48.0	) feet.		Щ				
7 CS	100		50 -	LIME		ery weathe	red, light gra	y (10YR 7/1), m							
				End o	of boring at	t 55.0 feet	below groun	d surface.			-		200	2	
		( A		1	Transfer Control										

Facilit	y/Proje	ct Nam						Date Drilling Started	:	Date Dri			ted:		e 1 of 1 lect Number:
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Orilling	g Firm:	5.00			Drilling M			Surface Elev. (ft)	60.00	levation	(ft)	Total		(ft bgs	Borehole Dia.
2017			Drillin			Sonic		579.44	5	81.81			55.0		6
Boring	Locati	on: S	of fly as	h basin.				Personnel Drilling Equipment:  Logged By - Jennifer Reed						9	
N: 14	0938.	78 E:	1339	6986.03				Driller - Austin Gold						Terr	aSonic
Civil T	own/Ci	ty/or Vi	llage:	County:		State:		Water Level Observ						_	an character
	Monro	e, M	į.	М	onroe	Michig	gan	While Drilling: After Drilling:	Date/	Time	3/17/	16 09:3	3		pth (ft bgs) pth (ft bgs) -4.82
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AND TYPE	RECOVERY (%)	BLOW COUNTS	DEPTH IN FEET				OLOGIC RIPTION				nscs	GRAPHIC LOG	WELL DIAGRAM		COMMENTS
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S	95		10-	Chang Chang	e to very	at 9.5 feet stiff at 10.5 fee gray (10YR 4/1 at 12.0 feet.		l with light reddi	sh						
			20-								CL-				
T	65		-								ML				
S	100		4.3	Chang	e to no m	ottling at 25.0 f	eet.								
ī	95		30-												
S	100														
			40-									1/1		2	
S	100		- 0	coarse moist,	sand, low very stiff.	plasticity, dark	k gray (10	ome silt, little fin IYR 4/1), no odd dor at 42.5 feet.	e to or,		CL- ML				
			50-	plastic	ity, light gr	stly clay, some ay (10YR 7/1), ot cohesive at	slight od	gravel, very low or, moist, hard.			CL- ML				
S	100			LIMES	TONE we	athered, slight	odor, sat	urated.							
			60 —	End of	boring at	60.0 feet belov	v ground	surface.				İ			

acility	/Projec	t Name			7216	Date Drilling Started:	Date	Drilling		ted:	Project Number:	
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rilling	Firm:	took !	Orilling	100	g Method: Sonic	577.29	579.		Total	50.0		
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	/lonro	e Mi		Monroe	Michigan	While Drilling: After Drilling:	Date/Time		/16 09:2	5	Depth (ft bgs) Depth (ft bgs) -13.95	
SAM	_			:	1			T				
AND TYPE	RECOVERY (%)	BLOW COUNTS	DEPTH IN FEET		LITHOLOG DESCRIPT			nscs	GRAPHIC LOG	WELL DIAGRAM	COMMENTS	
S	70		1 1 1	brown (10YR organics, roo Change to no	mostly clay, some silt, 2/2), no odor, moist, mots. o roots, trace fine grave ood fragments present	edium stiff (2.0 tsf), I at 2.5 feet.	ark high				Artesian well conditions present.	
1			10-		edium to high plasticity	1)	1111					
S	60			mottled with (5YR 6/3), no Change to tra gravel low pla	yellowish brown (10YR) o organics at 10.0 feet. ace to few fine to coarse asticity, yellowish brown ark gray (10YR 4/1), ve	5/6) and light reddis e sand, trace to few n (10YR 5/4), at 12.0	h brown fine feet.	CL-				
T	100		20-					ML				
i S	100		30 —	Change to ha	ard (>4.0 tsf) at 30.0 fee	ət.						
S	100		1	SAND most	y fine to coarse sand, ti	race to fourcilt very	dark	- 00				
			40-	gray (10YR 3	3/1), no odor, moist, loo	se.	,	SP CL-	W			
S	100		40	SILTY CLAY (10YR 4/1), r LIMESTONE saturated. Change to ve	mostly clay, some silt, no odor, moist, very stif- light gray (10YR 7/1), ery weathered, moist at ompetent, dry.	low plasticity, dark of (3.0 tsf). slight odor, weathere 41.0 feet.	1	ML				
			4	Elia oi porin	g at 50.0 feet below gro	unu sullace.						

Facili	ty/Projec	rt Nam	o.				Date Drilling Started		Date Drillir	a Co	mnlata	d.	Page 1	of 1 t Number:
auil	cyrr rujec	or i vaill		DTE EC: Mor	roe FAF	1	2/15/16			15/1		u.		828.0001.
Drillin	g Firm.				rilling Metho		Surface Elev. (ft)	TOCE	evation (ft		2	epth (	ft bgs)	Borehole Dia
	S	tock	Drillin	Control of the		Sonic	582.64	000000	35.54			50.0		6
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N: 1	40704.6	67 E	1339	0758.97			Logged By - Chris Driller - Austin Gold						Terra	Sonic
Civil	Fown/Cit	ty/or Vi	llage:	County:		State:	Water Level Observ While Drilling:	ations:	Timo				Dont	h (ft bgs)
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			3	Change to	soft (0.	5 tsf) at 10.0 feet.								
2 CS	100		-	Change to	very stil	ff (3 to 4 tsf) at 15.	0 feet.							
3 ST	80		20-			ay (10YR 4/1) at 1			CL					
4			-	Change to	very stil	if to hard (3 to >4 t	sf) at 22.0 feet.							
4 CS	100		-											
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5 CS	100			5										
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	8			\saturated,	medium	dense to dense.			SI	1		E.		
6 CS	80			_∖gray (10YF ∖dense.	R 5/1), n	o odor, moist to sa	sand, little to some turated, dense to v	ery	М	-		目		
			50-	grayish bro	own (10)	(R 4/2), no odor, d	nd, no plasticity, dar ry, very dense. c gray (10 R 4/1), di		_/_		国			
			1	competent	but frac		2	21	_/					

,,						12 30 20 30					Page 1	
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Borino				g fly ash basin, along f	and the second s	Personnel	100	00.20	Drillin	g Equip		6
					97.550 W. 30 T. 3.7 <b>4</b> 50 ° °	Logged By - Jenn		i i				Conin
	9537.1 own/Cit	1		2810.51 County:	State:	Driller - Austin Go Water Level Obser	7 172 177 1		1		rerra	Sonic
				Monroe		While Drilling:	Date.	/Time	40.40			h (ft bgs)
	Monro	be, IVI		Monroe	Michigan	After Drilling:	Date	/Time _ <u>5/5</u>	16 12:47		Depti	h (ft bgs) -16.70
OAIV												
NUMBER AND TYPE	RECOVERY (%)	BLOW COUNTS	DEPTH IN FEET		LITHOLOG DESCRIPT	TION		USCS	GRAPHIC LOG	WELL DIAGRAM	С	COMMENTS
1 CS	75		10-	dark brown (* material pres Change to fe Change to br 5.0 feet.	mostly clay, little to so 10YR 2/2), no odor, motent, roots and grass. w to little fine to coarse own (10YR 5/3), very sace to few gravel, gray	oist, medium stiff, or e sand at 2.5 feet. stiff, no organic mat	rganic erial at				Artesia	in well conditions it.
2 CS	100		20-					CL				
3	100		9 1 1 1									
4 CS	100		30-	Change to no (10YR 4/1), h	o to trace fine to mediu nard at 30 feet.	m sand, no gravel,	dark gr	ay				
-			40-	LIMESTONE	weathered, light gray	(10YR 7/1), slight o	dor.		1	1		
			4	moist to dry.			No.		T	相		
5	172		-						1	1日		
ČS	100		-	Change to co	ompetent at 46.5 feet.				H	16		
			4	onange to co	impotent at 40.0 ledt.				$\perp$			
			50 —	End of boring	g at 50.0 feet below gro	ound surface			-	10.0	4	
			-	End of boiling	g at 50.0 leet below git	Juna Suriace.						
			1									

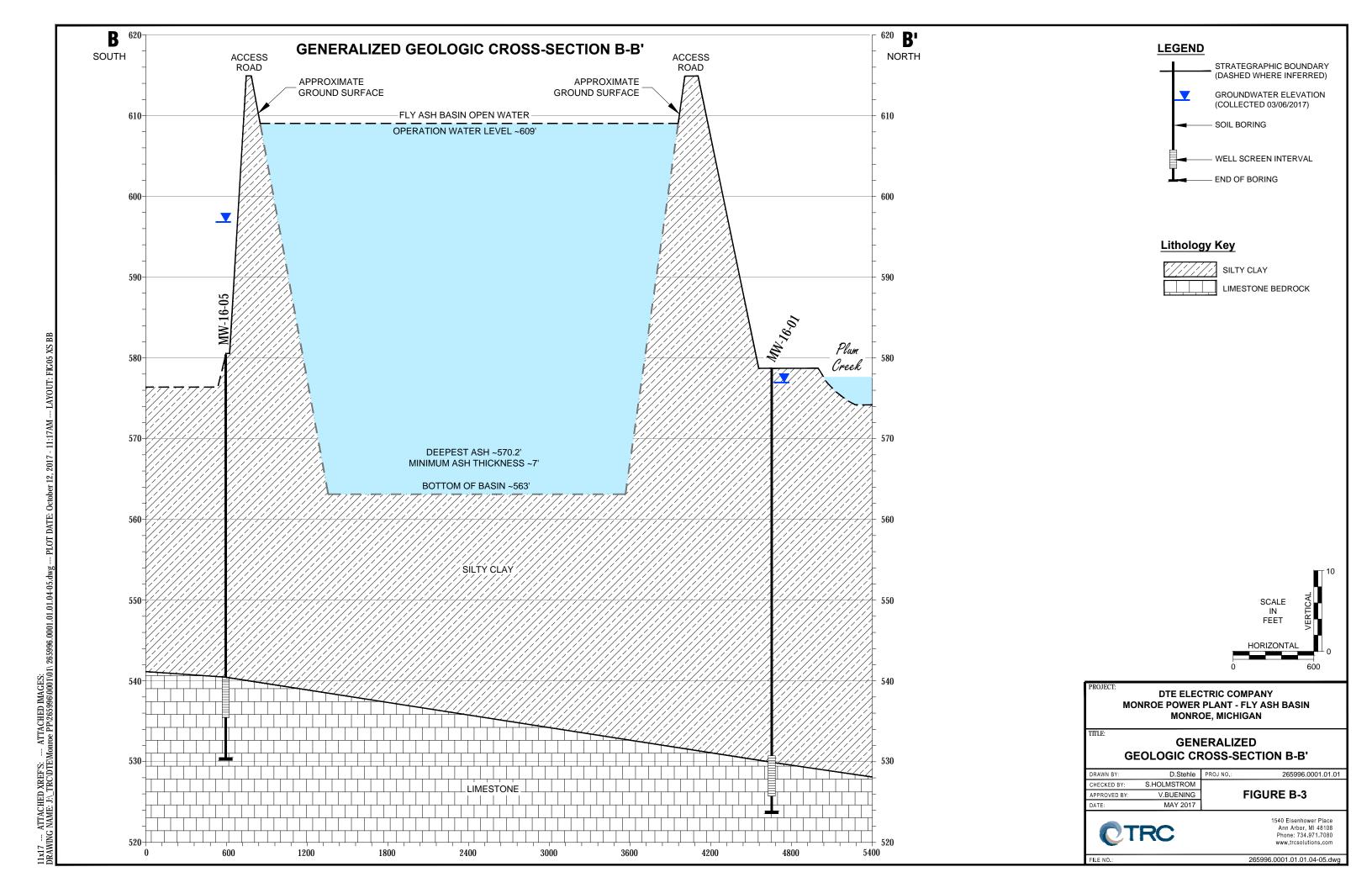
ject Nan				Date Drilling Started	d: Da	te Drilling	Complete	ed:	Project	Number:
		DTE EC: Monroe	FAB	4/13/16		4/1:	3/16			28.0001.00
n.		Drilling I	Method.	Surface Elev. (ft)	TOC Elev	ation (ft)	Total D	epth (ft	bgs)	Borehole Dia. (
			Sonic	579.20	581	.94				6
ation: N	IE of fly	ash basin, along the rive	r's edge.	Personnel	fer Reed		Drilling	Equipn	nent:	
6.72 E	: 1339	6398.37						1	Terra S	Sonic
City/or \	fillage:	County:	State:			200			A 1.57	WY V
roe. N	11	Monroe	Michigan				6 09:30			(ft bgs) (ft bgs) <u>-3.45</u>
				J			T			(1-5-7 3-3-3
BLOW COUNTS	DEPTH IN FEET		DESCRIPTI	ON		SSCS	GRAPHIC LOG	WELL DIAGRAM	С	OMMENTS
		coarse sand, fe medium stiff, h	ew to little clay, black ( igh organic content, ro	(10YR 2/1), no odo oots and grass.		ML- CL				well conditions
	10-	sand, light yello Change to brow Change to dark Change to no t	owish brown (10YR 6/- vn (10YR 5/3), very st c gray (10YR 4/1), har o trace sand at 15.0 fo	4), moist, medium s iff to hard at 7.0 fee d at 11.5 feet. eet.	stiff. et.	CL- ML				
ir.	20-				ne to					
						CL- ML				
	50 —	GRAVEL AND and cobbles, s	COBBLES large brok aturated.	en limestone bould	ders,	GP				
	ation: N 5.72 E City/or V roe, N SLNn00 MO18	ation: NE of fly: 3.72 E: 1339 City/or Village: roe, MI  LEBURY ON MONTH AND	CLAYEY SILTY Coarse sand, femedium stiff, horage to very silty CLAY mand, light yello Change to brown and, light yello Change to not silty CLAY works and, of the coarse sand, described by the coarse sand, described b	ation: NE of fly ash basin, along the river's edge.  3.72 E: 13396398.37  Citylor Village: County: State: roe, MI Monroe Michigan  LITHOLOG DESCRIPTI  CLAYEY SILT WITH SAND mostly si coarse sand, few to little clay, black medium stiff, high organic content, rown change to very dark gray (10YR 3/1)  SILTY CLAY mostly clay, some silt, sand, light yellowish brown (10YR 6/4)  Change to dark gray (10YR 4/1), hare  Change to dark gray (10YR 4/1), hare  Change to no to trace sand at 15.0 ference sand, dark gray (10YR 4/1), rown coarse sand, dark gray (10YR 4/1), rown	Attor: NE of fly ash basin, along the river's edge.  1.72 E: 13396398.37  Citylor Village: County: State: Water Level Obser While Drilling: After Drilling: Af	Ation: NE of fly ash basin, along the river's edge.  1.72 E: 13396398.37  Citylor Village: County: State: White Drilling: Date/Tin After Drilling: Date/Tin Descriptions  1. CLAYEY SILT WITH SAND mostly slit, few to little fine to coarse sand, few to little clay, black (10YR 2/1), no odor, moist, medium stiff, high organic content, roots and grass. Change to very dark gray (10YR 3/1) at 2.5 feet.  1. SILTY CLAY mostly clay, some silt, few to little fine to coarse sand, light yellowish brown (10YR 6/4), moist, medium stiff. Change to dark gray (10YR 4/1), hard at 11.5 feet.  1. Change to dark gray (10YR 4/1), hard at 11.5 feet.  1. Change to no to trace sand at 15.0 feet.  3. SILTY CLAY WITH SAND mostly clay, some silt, little fine to coarse sand, dark gray (10YR 4/1), moist, hard.  3. GRAVEL AND COBBLES large broken limestone boulders, dark gray (10YR 4/1), moist, hard.	Allor: NE of fly ash basin, along the river's edge.  1.72 E: 13396398.37    Cliv/or Village:   County:   State:   Water Lavel Observations:   Date/Time   StS/1   Water Lavel Observations:   Water Lavel Observations:   White Diffling:   Date/Time   StS/1   Water Lavel Observations:   Water Lavel Observations:   White Diffling:   Date/Time   StS/1   Water Lavel Observations:   Water Lavel Observations:   White Diffling:   Date/Time   StS/1   Water Lavel Observations:   Water Lavel Observations:   White Diffling:   Date/Time   StS/1   Water Lavel Observations:   Date/Time   StS/1   LTT HOLOGIC   DESCRIPTION   Water Lavel Observations:   Water Lavel Observations:   StS/1   CLAYEY SILT WITH SAND mostly slit, few to little fine to coarse sand, light yellowish brown (10YR 3/1) at 2.5 feet.   SiLTY CLAY mostly clay, some slit, few to little fine to coarse sand, light yellowish brown (10YR 6/4), moist, medium stiff.   Change to brown (10YR 5/3), very stiff to hard at 7.0 feet.   CL-ML   C	ation: NE of fly ash basin, along the river's edge.  5.72 E: 13396398.37    State:	ation: NE of fly ash basin, along the river's edge.  7.72 E: 13398398.37    Personnel Logged By - Jennifer Read Driller - Austin Goldermith Drilling Equipment of the Property	Size E: 13396398.37  Clover Village: County: State: Water Level Observations: Depth

Enaille	u/Droin	of Man				1.	Ooto Dellina Ctdd	. 15		ELL		Page 1 of 1
racilit	y/Projec	a Name		DTE EC: Monro	eFΔR	,	Date Drilling Started 4/14/16	.  0	ate Drilling	Comple 4/16	tea:	Project Number: 231828.0001.00
Drilling	g Firm:				g Method:	5	Surface Elev. (ft)	TOC Ele	vation (ft)		Depth	(ft bgs)   Borehole Dia. (
			Drillin	g	Sonic		575.41	57	8.40		40.0	The state of the state of the state of
Boring	Location Location	on: N	of fly as	sh basin, S of E Dunb	ar Road, W of main gate.		Personnel Logged By - Jennif	er Reed		Drillin	g Equip	pment:
				2311.01	12		Driller - Austin Gold	dsmith				TerraSonic
	own/Cit			County:	State:		Vater Level Observ While Drilling:	ations: Date/Ti	me			Depth (ft bgs)
_	Monro	e, M		Monroe	Michiga	an	After Drilling:	Date/Ti	me <u>5/5/1</u>	6 10:44		Depth (ft bgs)
SAIV	PLC											
NUMBER AND TYPE	RECOVERY (%)	BLOW COUNTS	DEPTH IN FEET			DLOGIC RIPTION			nscs	GRAPHIC LOG	WELL DIAGRAM	COMMENTS
1 3	95			(10YR 5/3) to	mostly clay, some gray (10YR 5/1), r	no odor, m	oist, medium s	own stiff.				Artesian well conditions present.
2	100								CL- ML			
3 88	100		30-	dark gray (10 Change to lit	WITH CLAY mostl DYR 4/1), moist, me tle to some sand at ray (GLEY1 5/N), co	edium to ve t 25.0 feet.	ery stiff.	у,	ML- CL			
4	100				et at 35.0 feet.							
				wet.	weathered, light g	gray (10YR	7/1), slight od	or,		H	目	
			40 —	Change to sa	aturated at 39.5 fee	et.	urfanc		1			
			1	End of boring	g at 40.0 feet below	v grouna s	ипасе,					
			-									
			-									
			50-									
			-						4			
			-									
		Λ										
igna	wre:	1	(	La Sor	Firm		nvironmental (	Corpora	tion Arbor,			734-971-70

# Appendix B Cross Sections



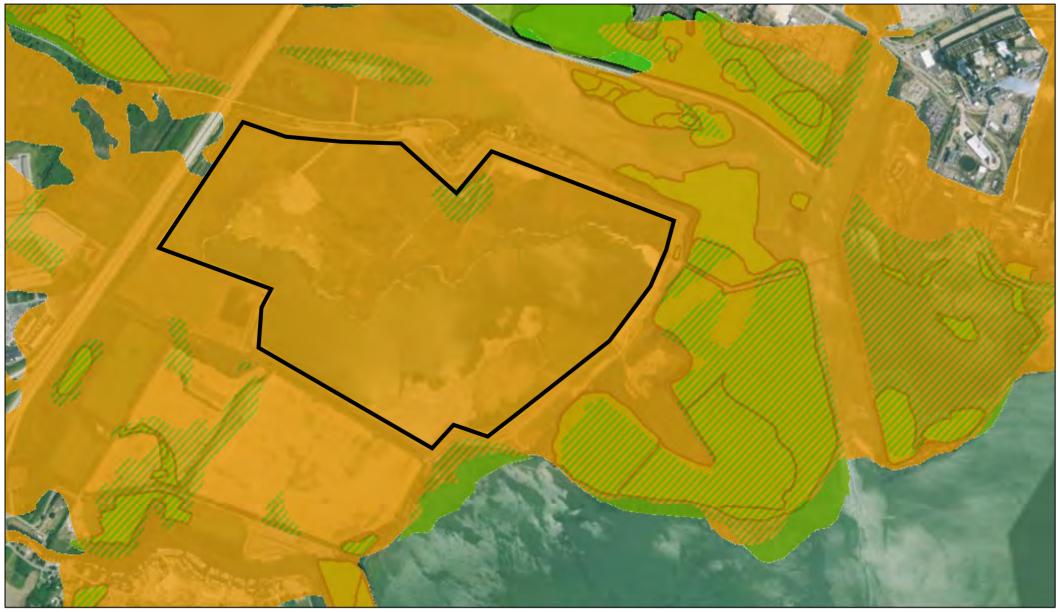
#### **LEGEND GENERALIZED GEOLOGIC CROSS-SECTION A-A'** STRATEGRAPHIC BOUNDARY (DASHED WHERE INFERRED) GROUNDWATER ELEVATION (COLLECTED ON 03/06/2017) Α' A SOIL BORING WEST EAST 590-590 WELL SCREEN INTERVAL \_\_\_\_ END OF BORING APPROXIMATE GROUND SURFACE 580-580 Lithology Key CLAYEY SILT / **CLAYEY SILT** SILTY CLAY SANDY SILT WITH CLAY LIMESTONE GRAVEL / COBBLES APPROXIMATE ELEVATION OF BOTTOM OF FLY ASH BASIN LIMESTONE BEDROCK SILTY CLÁY 560 SILTY CLAY WITH CLAY SCALE LIMESTONE IN GRAVEL/COBBLES FEET **HORIZONTAL** DTE ELECTRIC COMPANY MONROE POWER PLANT - FLY ASH BASIN MONROE, MICHIGAN 600 1200 1800 2400 3600 4200 4800 5400 3000 **GENERALIZED GEOLOGIC CROSS-SECTION A-A'** D.STEHLE PROJ NO.: 265996.0001.01 DRAWN BY: S.HOLMSTROM APPROVED BY: V.BUENING FIGURE B-2 SEPTEMBER 2017 1540 Eisenhower Place Ann Arbor, MI 48108 Phone: 734.971.7080 www.trcsolutions.com 265996.0001.01.01.04-05.dwg



## Appendix C National Wetland Inventory Map



## Wetlands Map Viewer



August 17, 2018

Part 303 Final Wetlands Inventory

Wetlands as identified on NWI and MIRIS maps and soil areas which include wetland soils

Wetlands as identified on NWI and MIRIS maps

Gage Stations

Soil areas which include wetland soils

National Wetlands Inventory 2005

1:15,382

0 0.125 0.25 0.5 mi

0 0.2 0.4 0.8 km

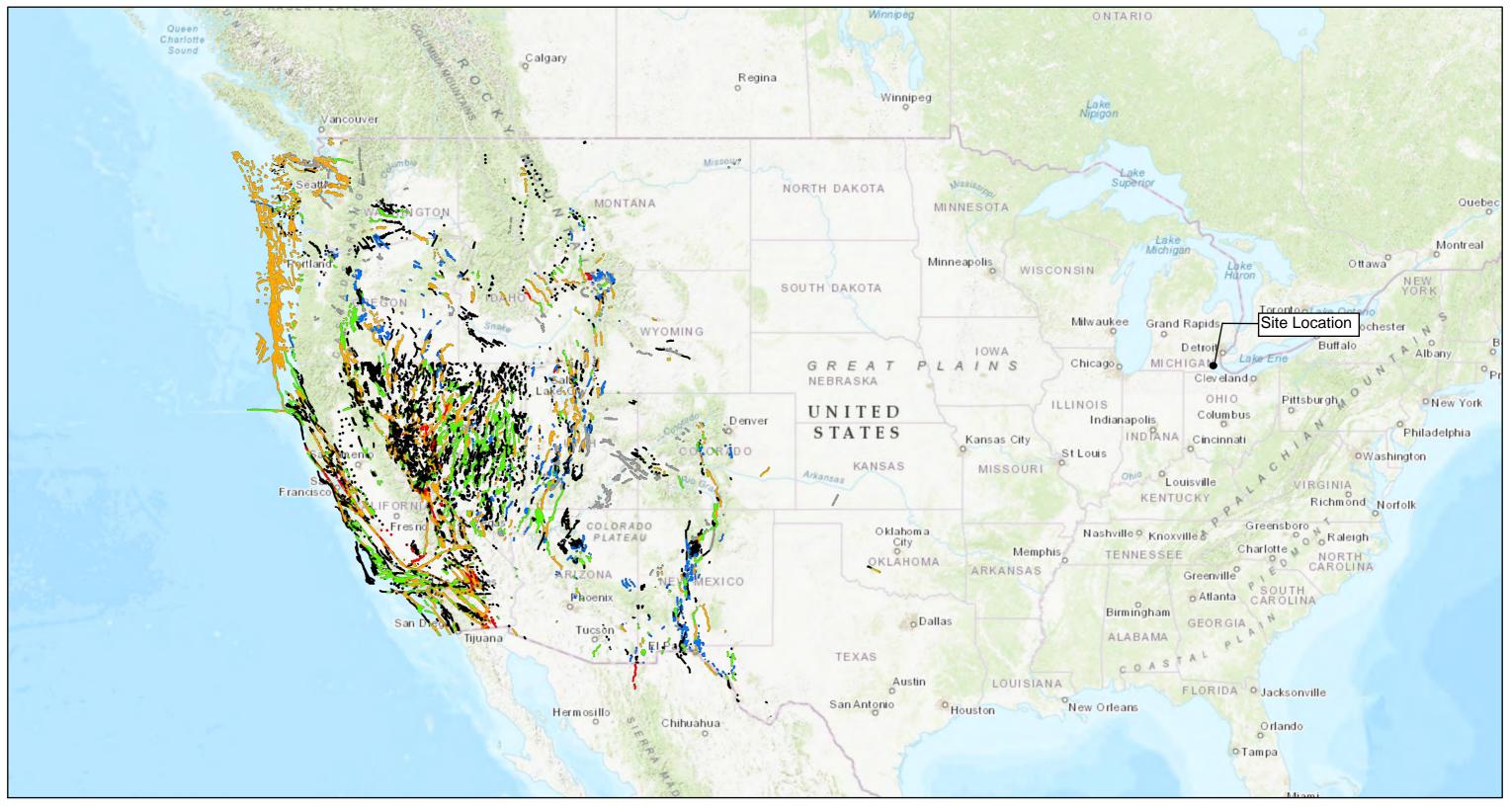
Sources: Esri, HE RE, Gamin, USGS, Intermap, INCREMENT P, NRCan, Esri
Japan, METI, Esri China (Hong Kong), Esri Korea, Esri (Thailand), NGCC, ©

OpenStreetMap contributors, and the GIS User Community

# Appendix D U.S. Quaternary Faults and Folds Map



## US Quaternary Faults and Fdds



#### 97/2018 32039PM

#### Quaternary faults

- unspecified age, well constrained location
- -- unspecified age, moderately constrained location
- " unspecified age, inferred location
- undifferentiated Quaternary (< 130,000 years), well constrained location</li>
- " undifferentiated Quaterrary (< 130,000 years), moderately constrained location \_\_\_
- undifferentiated Quaterrary (< 130,000 years), inferred location
- middle and late Quaterrary (< 1.6 million years), well constrained location
- middle and late Quaterrary (< 1.6 million years), moderately constrained location
- " middle and late Quaterrary (< 1.6 million years), inferred location
- latest Quaternary (<15,000 years), well constrained location
  - latest Quaternary (<15,000 years), moderately constrained location

" latest Quaternary (<15,000 years), inferred location

late Quaternary (< 130,000 years), well constrained location

## 1:18,489,298 O 175 350 700mi O 275 550 1,100km

Sources Esri, HERE, Garmin, Intermap, increment P.Corp., GEBCO, USGS, FAO, NPS, NRCAN, GeoBæse, IGN, Kadester NL, Ordhance Survey, Esri Japan, METI, Esri China (Hong Kong), svisstopo, © OpenStreetNapcontributors, and the GIS User Community, USGS

# Appendix E U.S. Seismic Design Maps



#### U.S. Geological Survey - Earthquake Hazards Program

Due to insufficient resources and the recent development of similar web tools by third parties, this spring the USGS will be streamlining the two U.S. Seismic Design Maps web applications, including the one below. Whereas the current applications each interact with users through a graphical user interface (GUI), the new web services will receive the inputs (e.g. latitude and longitude) in the form of a web address and return the outputs (e.g.  $S_{DS}$  and  $S_{D1}$ ) in text form, without supplementary graphics. Though designed primarily to be read by the aforementioned third-party web GUIs, the text outputs are also human-readable. To preview the new web services, please click here. Step-by-step instructions for using one of these web services, namely that for the recently published 2016 ASCE 7 Standard, are posted here.

## **MONPP FAB - Seismic Impact Zone**

Latitude = 41.884°N, Longitude = 83.375°W

Location



Reference Document

2015 NEHRP Provisions

Site Class

C: Very Dense Soil and Soft Rock

**Risk Category** 

I or II or III

 $S_S = 0.122 g$ 

0.050 g

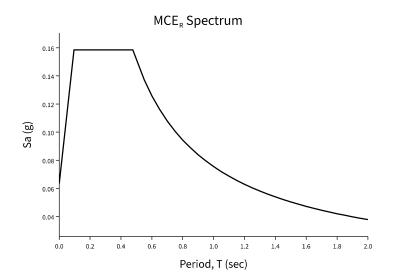
 $S_1 =$ 

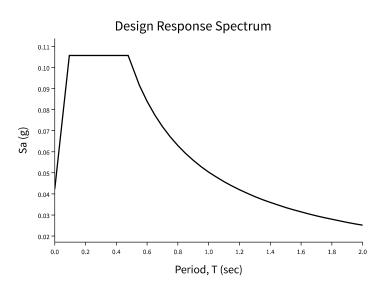
 $S_{MS} = 0.158 g$ 

 $S_{DS} = 0.106 g$ 

 $S_{M1} = 0.076 g$ 

 $S_{D1} = 0.050 g$ 





### Mapped Acceleration Parameters, Long-Period Transition Periods, and Risk Coefficients

Note: The  $S_S$  and  $S_1$  ground motion maps provided below are for the direction of maximmum horizontal spectral response acceleration. They have been converted from corresponding geometric mean ground motions computed by the USGS by applying factors of 1.1 (to obtain  $S_S$ ) 1.3 (to obtain  $S_1$ ).

- <u>FIGURE 22-1 S<sub>S</sub> Risk-Targeted Maximum Considered Earthquake (MCE<sub>R</sub>) Ground Motion Parameter</u>
   <u>for the Conterminous United States for 0.2 s Spectral Response Acceleration (5% of Critical Damping), Site Class B</u>
- <u>FIGURE 22-2 S<sub>1</sub> Risk-Targeted Maximum Considered Earthquake (MCE<sub>R</sub>) Ground Motion Parameter for the Conterminous United States for 1.0 s Spectral Response Acceleration (5% of Critical Damping), Site Class B</u>
- FIGURE 22-9 Maximum Considered Earthquake Geometric Mean (MCE<sub>G</sub>) PGA, %g, Site Class B for the Conterminous United States
- FIGURE 22-14 Mapped Long-Period Transition Period, T<sub>1</sub> (s), for the Conterminous United States
- FIGURE 22-18 Mapped Risk Coefficient at 0.2 s Spectral Response Period, C<sub>RS</sub>
- FIGURE 22-19 Mapped Risk Coefficient at 1.0 s Spectral Response Period, C<sub>R1</sub>

### **Site Class**

The authority having jurisdiction (not the USGS), site-specific geotechnical data, and/or the default has classified the site class as Site Class, based on the site soil properties in accordance with Chapter 20.

Table 20.3-1 Site Classification

Site Class	- v <sub>S</sub>	$\overline{N}$ or $\overline{N}_{ch}$	- s <sub>u</sub>								
A. Hard Rock	>5,000 ft/s	N/A	N/A								
B. Rock	2,500 to 5,000 ft/s	N/A	N/A								
C. Very dense soil and soft rock	1,200 to 2,500 ft/s	>50	>2,000 psf								
D. Stiff Soil	600 to 1,200 ft/s	15 to 50	1,000 to 2,000 psf								
E. Soft clay soil	<600 ft/s	<15	<1,000 psf								
	<ul> <li>Any profile with more than 1</li> <li>Plasticity index PI &gt; 20</li> <li>Moisture content w ≥ 40</li> <li>Undrained shear streng</li> </ul>	0% <u>,</u> and	ne characteristics:								
F. Soils requiring site response analysis in accordance with Section 21.1		See Section 20.3.1									
For SI: 1	Lft/s = $0.3048 \text{ m/s } 1 \text{lb/ft}^2 = 0.0479$	For SI: $1 \text{ft/s} = 0.3048 \text{ m/s} 1 \text{lb/ft}^2 = 0.0479 \text{ kN/m}^2$									

## Site Coefficients and Risk-Targeted Maximum Considered Earthquake ( $MCE_R$ ) Spectral Response Acceleration Parameters

Risk-targeted Ground Motion (0.2 s)

 $C_{RS}S_{SUH} = 0.950 \times 0.128 = 0.122 g$ 

Deterministic Ground Motion (0.2 s)

 $S_{SD} = 1.500 g$ 

 $S_S \equiv$  "Lesser of  $C_{RS}S_{SUH}$  and  $S_{SD}$ " = 0.122 g

Risk-targeted Ground Motion (1.0 s)

 $C_{R1}S_{1UH} = 0.903 \times 0.056 = 0.050 \text{ g}$ 

Deterministic Ground Motion (1.0 s)

 $S_{1D} = 0.600 g$ 

 $S_1 \equiv$  "Lesser of  $C_{R1}S_{1UH}$  and  $S_{1D}$ " = 0.050 g

### Table 11.4-1: Site Coefficient Fa

	Spectral Repo	Spectral Reponse Acceleration Parameter at Short Period										
Site Class	S <sub>S</sub> ≤ 0.25	S <sub>S</sub> = 0.50	S <sub>S</sub> = 0.75	S <sub>S</sub> = 1.00	S <sub>S</sub> = 1.25	S <sub>S</sub> ≥ 1.50						
А	0.8	0.8	0.8	0.8	0.8	0.8						
B (measured)	0.9	0.9	0.9	0.9	0.9	0.9						
B (unmeasured)	1.0	1.0	1.0	1.0	1.0	1.0						
С	1.3	1.3	1.2	1.2	1.2	1.2						
D (determined)	1.6	1.4	1.2	1.1	1.0	1.0						
D (default)	1.6	1.4	1.2	1.2	1.2	1.2						
Е	2.4	1.7	1.3	1.2 *	1.2 *	1.2 *						
F		'	See Sec	tion 11.4.7								

<sup>\*</sup> For Site Class E and  $S_S \ge 1.0$  g, see the requirements for site-specific ground motions in Section 11.4.7 of the 2015 NEHRP Provisions. Here the exception to those requirements allowing  $F_a$  to be taken as equal to that of Site Class C has been invoked.

Note: Use straight-line interpolation for intermediate values of S<sub>S</sub>.

Note: Where Site Class B is selected, but site-specific velocity measurements are not made, the value of  $F_a$  shall be taken as 1.0 per Section 11.4.2.

Note: Where Site Class D is selected as the default site class per Section 11.4.2, the value of  $F_a$  shall not be less than 1.2 per Section 11.4.3.

For Site Class = C and  $S_S = 0.122 g$ ,  $F_a = 1.300$ 

Table 11.4-2: Site Coefficient F<sub>v</sub>

	Spectral Response Acceleration Parameter at 1-Second Period										
Site Class	S <sub>1</sub> ≤ 0.10	S <sub>1</sub> = 0.20	S <sub>1</sub> = 0.30	S <sub>1</sub> = 0.40	S <sub>1</sub> = 0.50	S <sub>1</sub> ≥ 0.60					
А	0.8	0.8	0.8	0.8	0.8	0.8					
B (measured)	0.8	0.8	0.8	0.8	0.8	0.8					
B (unmeasured)	1.0	1.0	1.0	1.0	1.0	1.0					
С	1.5	1.5	1.5	1.5	1.5	1.4					
D (determined)	2.4	2.2 1	2.0 <sup>1</sup>	1.9 <sup>1</sup>	1.8 1	1.7 1					
D (default)	2.4	2.2 1	2.0 <sup>1</sup>	1.9 <sup>1</sup>	1.8 1	1.7 1					
Е	4.2	3.3 <sup>1</sup>	2.8 1	2.4 <sup>1</sup>	2.2 1	2.0 <sup>1</sup>					
F			See Sect	ion 11.4.7							

 $<sup>^{1}</sup>$  For Site Class D or E and S<sub>1</sub> ≥ 0.2 g, site-specific ground motions might be required. See Section 11.4.7 of the 2015 NEHRP Provisions.

Note: Use straight-line interpolation for intermediate values of S<sub>1</sub>.

Note: Where Site Class B is selected, but site-specific velocity measurements are not made, the value of  $F_v$  shall be taken as 1.0 per Section 11.4.2.

For Site Class = C and 
$$S_1 = 0.050 g$$
,  $F_V = 1.500$ 

Site-adjusted MCE<sub>R</sub> (0.2 s)

$$S_{MS} = F_a S_S = 1.300 \times 0.122 = 0.158 g$$

Site-adjusted MCE<sub>R</sub> (1.0 s)

$$S_{M1} = F_v S_1 = 1.500 \times 0.050 = 0.076 g$$

## **Design Spectral Acceleration Parameters**

Design	Ground	Motion	(0.2 s)	
--------	--------	--------	---------	--

$$S_{DS} = \frac{2}{3} S_{MS} = \frac{2}{3} \times 0.158 = 0.106 g$$

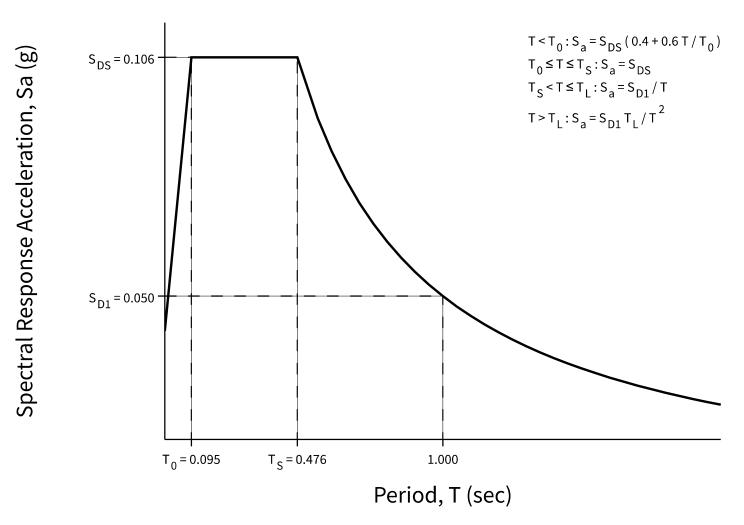
Design Ground Motion (1.0 s)

$$S_{D1} = \frac{2}{3} S_{M1} = \frac{2}{3} \times 0.076 = 0.050 g$$

## **Design Response Spectrum**

Long-Period Transition Period =  $T_L$  = 12 s

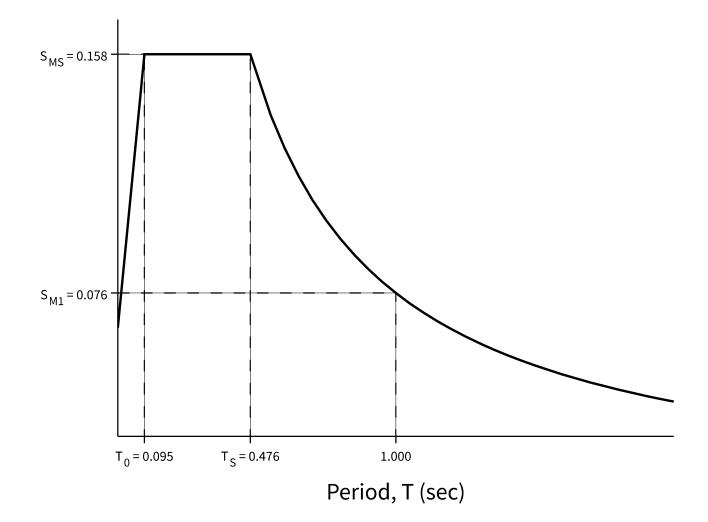
Figure 11.4-1: Design Response Spectrum



## MCE<sub>R</sub> Response Spectrum

The MCE<sub>R</sub> response spectrum is determined by multiplying the design response spectrum above by 1.5.





## Additional Geotechnical Investigation Report Requirements for Seismic Design Categories D through F

Table 11.8-1: Site Coefficient for F<sub>PGA</sub>

	Mapped MCE 0	apped MCE Geometric Mean (MCE <sub>G</sub> ) Peak Ground Acceleration						
Site Class	PGA ≤ 0.10	PGA = 0.20	PGA = 0.30	PGA = 0.40	PGA = 0.50	PGA ≥ 0.60		
А	0.8	0.8	0.8	0.8	0.8	0.8		
B (measured)	0.9	0.9	0.9	0.9	0.9	0.9		
B (unmeasured)	1.0	1.0	1.0	1.0	1.0	1.0		
С	1.3	1.2	1.2	1.2	1.2	1.2		
D (determined)	1.6	1.4	1.3	1.2	1.1	1.1		
D (default)	1.6	1.4	1.3	1.2	1.2	1.2		
Е	2.4	1.9	1.6	1.4	1.2	1.1		
F	See Section 11.4.7							

Note: Use straight-line interpolation for intermediate values of PGA

Note: Where Site Class D is selected as the default site class per Section 11.4.2, the value of  $F_{pga}$  shall not be less than 1.2.

## For Site Class = C and PGA = 0.063 g, $F_{PGA} = 1.300$

Mapped MCE<sub>G</sub>

PGA = 0.063 g

Site-adjusted MCE<sub>G</sub>

 $PGA_{M} = F_{PGA}PGA = 1.300 \times 0.063 = 0.082 g$